

Comparative Evaluation of the Influence of Cast Hardening Agents on Surface Abrasion, Surface Hardness and Surface Detail Reproduction Properties of Refractory Investment Materials

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ABSTRACT

To evaluate and compare the effectiveness of Dental Cast Hardening Agents on the Surface Abrasion, Surface Hardness and Surface Detail reproduction of Dental Refractory investment materials. This study utilised two commercially available refractory materials: Rema exakt Dentaureum (Germany), X20 chrome investment whip mix corporation (U.S.A). The samples were divided into four groups: Group I- Untreated samples, Group II- Samples treated with paraffin wax, Group III- Samples treated with bees wax, Group IV- Samples treated with okodur cold hardener. Surface abrasion test was done by electrically operated abrading tool, surface hardness by Mohs' scale, surface details with Galai scan array 2 image system. Mean difference were statistically analysed using students t test. For Surface abrasion test, all groups showed statistically significant difference (<0.01) except Group 2 samples of X20 chrome refractory investment material compared with Group 3 and 4 (>0.05). Mohs' Scale value for the Group 4 samples were the hardest with a value of five. Results of the surface reproducibility showed that both untreated and treated samples showed a reduced width of the groove, when compared with the steel model. Results of test for surface abrasion and surface hardness indicated that hardening agents do improve the surface abrasion resistance and abrasion values of treated samples.

Keywords: Surface roughness, Surface hardness, Surface details, Refractory Investment.

INTRODUCTION

The Dental refractory investments are used to achieve working refractory model by duplicating the master cast which has a definite disadvantage of providing an easily abradable and roughened surface for the model. This can be attributed to the larger particle size of the refractory material used in the investment. To prevent the surface of the duplicated master model from being abraded and to preserve the duplicated details and to provide a

smooth and harder surface for working, the refractory models are treated with Dental hardeners.¹⁻² These hardeners get readily absorbed in to the surface of the refractory models and also seal the surface pores. Cast hardeners are thus said to improve the surface hardness, preserve surface details and bring about better adherence and adaptability of pattern wax on the refractory models. The various properties of die materials investments, casting alloys and various techniques have been evaluated, perfected, and reported.³⁻⁷ The variations in binder content,

refractory agents and heat treatment may lead to changes in strength properties and also the various hardening agents available commercially claim to improve the working characteristics of the refractory models along with surface abrasion resistance and hardness.⁸⁻¹¹ This study was therefore proposed with following objectives

1. To evaluate and compare the surface abrasion resistance of refractory cast investment materials before and after cast hardening.
2. To determine and compare the surface hardness of refractory cast investment materials before and after cast hardening.
3. To compare the surface reproduction property of refractory cast investment materials before and after cast hardening.

MATERIALS AND METHODS

Various different brands of investment materials are in use for constructing refractory models. Commercially available refractory materials and hardeners used in the study are shown in Table I.



Fig. 1: Silicon Mould Using Reprosil Putty

Preparation of samples of Refractory Investment Materials

An acrylic block measuring 5x2x1cms was used to prepare the silicon mold (Reprosil putty consistency, Dentsply) (Figure 1). Twenty rectangular blocks (Figure 2) each measuring 5x2x1cms of both, the refractory investment materials were prepared following the recommended powder liquid ratio.

Rema exkat	400 grams : 56ml
X20 chrome investment	400 grams : 44ml

The required amount of powder and liquid were transferred into a mixing flask and hand spatulated for 15 seconds and then vacuum mixed following manufacturer's instructions. The vacuum mixed refractory investment material was then invested into preformed putty consistency molds. A steel disc of 4 cm in diameter with three lines 147.1580 microns width (Figure 3) engraved on it was duplicated using light body polysiloxane impression material (Reprosil, Dentsply U.S.A). Both the refractory investments were vacuum mixed following manufacturer instructions and were then

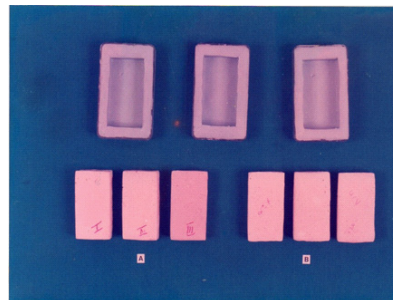


Fig. 2: Rectangular Blocks Made Of Refractory Investment Materials



Fig. 3: Steel Disc Of 4 Cm In Diameter With Three Lines 147.1580 Microns Width

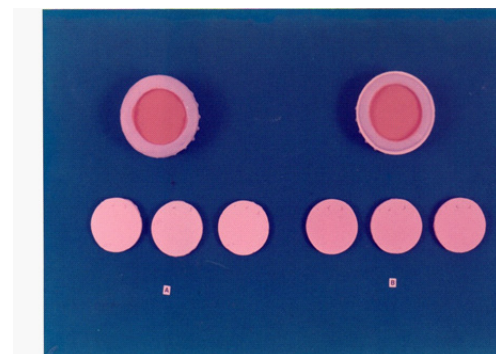


Fig. 4: After Drying And Hardening Treatment

invested in to these duplicated molds. After the lapse of thirty minutes, twenty samples were separated from the molds and were subjected to drying in a furnace and hardening treatment (Figure.4).

All twenty rectangular blocks and twenty round discs each of both the refractory investments were prepared for testing abrasion resistance, surface hardness and surface detail reproduction. The samples were then divided into four groups of five samples each: Group I- Untreated samples, Group II- Samples treated with paraffin wax, Group III- Samples treated with bees wax, Group IV- Samples treated with okodur cold hardener. Samples to be treated with paraffin wax were dipped in liquid paraffin for 10 seconds and drip dried. Bees wax was heated to 138-148 c and samples were dipped till the wax fumed and then drip dried. Samples treated with okodur cold hardener were dipped in cold hardener for 10 seconds and then returned to the furnace and heated at 170 c for 5 mins.

Testing For Surface Abrasion, Surface Hardness and Surface Detail Reproduction

Electrically operated metal shaping instrument with abrading tool contacting the samples 2 mm short of the borders and moved for a length of one and half inches (Figure 5). A sharp pointed tool made of high speed steel was used to abrade the samples. A force of 250 gram and depth of abrasion was maintained constant for all the samples. Twenty samples each of both the refractory investment material were numbered and then weighed using an electronic balance (precise 205A) which was sensitive to a weight of upto 0.01 mg. Each samples was subjected to an abrasion of four strokes of the abrading point at difference sites abraded samples were then carefully removed from the wise and the specimens were reweighed using the same electronic balance. The difference in the weight of all the samples before and after abrasion resistances testing was calculated. Hardness values for twenty samples of four groups of both the refractory investment materials used in the study were determined using Mohs' scale of scratch hardness (Figure 6).

Surface detail reproduction capacity of the untreated as well as hardened samples were determined by measuring the width of the duplicated groove in microns. This study utilized Galai scan array 2 image system with a block and white change coupled device video camera and reflected type optical microscope attached to a computer (Figure 7). The instrument is provided with a grid and smallest division in the grid corresponds a dimension of 6.689 microns. A mean of five readings made was taken as width of each groove. The differences in width was calculated by subtracting the width of the groove on

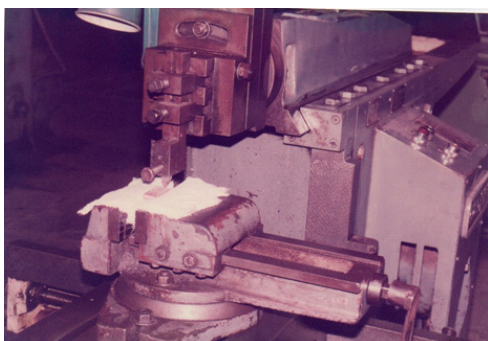


Fig. 5: Electrically Operated Metal Shaping Instrument For Testing Surface Abrasion



Fig. 6: Mohs' Scale Of Scratch Hardness



Fig. 7: Galai Scan Array Image System

the steel model (147.1580 microns). This difference was used to calculate mean and standard deviation for statistical analysis.

RESULTS

The mean of difference in weight of untreated samples before and after scraping range from 0.023-0.027gms for Rema exakt refractory investment and 0.023-0.27gms with x 20 chrome investment. The mean difference in weight of treated sample ranges from 0.012 – 0.022gms with Rema exakt refractory investment and 0.014 – 0.019gms with x 20 chrome investment. Statistical analysis of the mean values of weight loss for different groups of Rema Exakt and X20 chrome investment refractory material is shown in Table II and III. Hardness test for the samples of both the refractory investment materials, group I showed the least value of 3, Samples of group II and III were more harder than group I with a value of 4 and group IV was the

hardest, with a value of 5 on Mohs' scale (Table IV).

The mean difference in width of the samples with the width of the steel model were tabulated (Table V and VI) and statistically analysed using students t test. Significant difference was obtained ($P < 0.01$) with Group I samples of Rema exakt refractory investment materials when compared to Group II (t-value 6.0469) and III (t-value 6.9716). Significant difference ($p < 0.01$) was obtained with samples of Group II (t-value 6.8289) and Group III (t-value 7.8360) of the same refractory investment materials when compared with Group IV. Significant difference was observed on comparing Group I samples of x20chrome investment material with Group II (t-value 10.1164) and Group III (t-value 6.2146). Comparing mean difference in width of group II (t-value 4.4501) and Group III (t-value 3.6635) with values of group IV samples result obtained was significant difference ($p < 0.01$).

Table 1: Investment Materials And Hardners

Refractory Materials	Dental Cast Hardeners
1. Rema Exakt Dentaurum (Germany)	1. Paraffin wax
2. X20 Chrome Investment Whip Mix	2. Beeswax
3. Corporation (U.S.A).	3. Okodur cold hardener

Table 2: Comparison of means of differences in weight of Rema Exakt Refractory investment material in grams of groups

S. No	Groups	Mean	Standard Deviation	T-Value	P-Value	Significance
1	I	0.025	0.00159	3.7713	<0.01	Significant
	II	0.02	0.00212			
2	I	0.025	0.00159	5.7134	<0.01	Significant
	III	0.0156	0.00288			
3	I	0.025	0.00268	6.9299	<0.01	Significant
	IV	0.0142				
4	II	0.02	0.00212	2.4602	<0.05	Significant
	III	0.0156	0.00288			
5	II	0.02	0.00212	3.3939	<0.05	Significant
	IV	0.0142	0.00268			
6	III	0.0156	0.00288	0.7169	>0.05	Non significant
	IV	0.0142	0.00268			

DISCUSSION

Being very brittle and fragile in nature, the set phosphate or gypsum bonded refractory

investment model may be abraded during handling, wax pattern preparation and investing. Though the phosphate bonded investment attains adequate strength when heated during burnout, the refractory

Table 3: Comparison of means of differences in weight of X20 chrome investment Refractory investment material in grams of groups

S. No	Groups	Mean	Standard Deviation	T-Value	P-Value	Significance
1	I	0.0238	0.00259	4.8007	<0.01	Significant
	II	0.0166	0.00152			
2	I	0.0238	0.00259	4.6619	<0.01	Significant
	III	0.016	0.00212			
3	I	0.0238	0.00259	5.45121	<0.01	Significant
	IV	0.0154	0.00167			
4	II	0.0166	0.00152	0.46025	>0.05	Non significant
	III	0.016	0.00212			
5	II	0.0166	0.00152	1.0629	>0.05	Non significant
	IV	0.0154	0.00167			
6	III	0.016	0.00212	0.4418	>0.05	Non significant
	IV	0.0154	0.00167			

Table 4: MOH's Scale of hardness testing

	Sample No.	Hardness Number (Rema Exakt Refractory Investment material.)	Hardness Number (X20 chrome investment)
Unreated samples (Group I)	1	3	3
	2	3	3
	3	3	3
	4	3	3
	5	3	3
Treated with paraffin (Group II)	1	3	4
	2	3	4
	3	3	4
	4	3	4
	5	3	4
Treated with Beeswax (Group III)	1	4	4
	2	4	4
	3	4	4
	4	4	4
	5	4	4
Treated with Okodur (Group IV)	1	5	5
	2	5	5
	3	5	5
	4	5	5
	5	5	5

model should be protected from the surface being abraded.¹²⁻¹⁵

Abrasion resistance of the hardened samples were more than untreated samples. The thin layer of hardener formed on the surface of the samples seals the pores between the larger and coarser particles of investment material and there by prevents the direct contact of the abrading tool and resisting the removal of particles from the samples surface. The untreated samples on the other hand gets exposed to the tool and the pores present between the investment particles brings about easy removal of the investment from the samples surface.¹⁶⁻²¹

Hardness values can be considered to be related to the abrasion resistance and the values obtained shows that the hardness values on Mohs' scale was the highest for Group IV (hardness no.5) sample of both the refractory investment materials tested. Group II and Group III samples showed a higher value of hardness (Hardness no.4) when compared to untreated samples among both Rema exakt and X20 chrome investment materials. The values of hardness were the least for untreated samples (Hardness no.3) of the investments studied (Table V and VI).

The higher value of hardness among Group IV samples can be due to the inclusion of harder wax

Table 5: Comparison of difference in mean of width of the duplicated groove in Rema exakt refractory investment material

S. No	Groups	Mean In Microns	Standard Deviation	T-Value	P-Value	Significance
1	I	0.5351	0.4623	6.0469	<0.01	significant
	II	2.5873	0.6018			
2	I	0.5351	0.4623	6.9716	<0.01	significant
	III	2.9431	0.6187			
3	I	0.5351	0.4623	0.00032	>0.01	Non significant
	IV	0.535	0.2991			
4	II	2.5873	0.6018	0.9219	>0.01	Non significant
	III	2.9431	0.6187			
5	II	2.5873	0.6018	6.8289	<0.01	Significant
	IV	0.535	0.2991			
6	III	2.9431	0.6187	7.836	<0.01	Significant
	IV	0.535	0.2991			

Table 6: Comparison Of Difference In Mean Of Width Of The Duplicated Groove In X20 Chrome Investment Refractory Investment Material

S. No	Groups	Mean In Microns	Standard Deviation	T-Value	P-Value	Significance
1	III	1.07033.3954	0.36640.3605	10.1164	<0.01	significant
2	IIII	1.07033.2743	0.36640.7033	6.2146	<0.01	significant
3	IIV	1.07031.2487	0.36640.0168	0.3691	>0.01	Non significant
4	IIII	3.39543.2743	0.36050.7033	0.3435	>0.01	Non significant
5	IIIV	0.36051.2487	0.36050.0168	4.4501	<0.01	Significant
6	IIIV	3.27431.2487	0.70330.0168	3.6635	<0.01	Significant

in the reduced water powder ratio, thereby increasing the density of the material and also the mixture on vibration, the liquid content moves to surface leaving more amount of powder on the surface in apposition with the mold. This method of hardness testing has its limitations in being a relative measure of the hardness of the materials.

The measurements of the width of the groove reproduced showed that both the untreated and treated samples gave a reduced values of width of the grooves when compared with the steel model. the difference in width of the duplicated grooves of untreated samples with steel model can be attributed duplicating material, and inability of investment material itself, concentration of the liquid, and heat treatment procedure.²²⁻²⁵

Samples treated with hardeners also showed a difference in the width of the duplicated grooves, this can be due to the factors affecting the untreated samples and also because of the film of hardening agent being coated on the walls of the grooves, when the duplicating procedure and heat treatment is kept constant for both of the investment materials tested under similar conditions.

CONCLUSION

Comparing the available values it can be said that hardening agents do improve surface abrasion resistance and surface hardness of refractory investment materials, but these agents did mask the surface reproduction of the duplicated refractory model. However the practical implacability is not clear as partial dentures are being almost successfully constructed after treating with hardening agents.

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